Process Improvement: Steepest Ascent

BIOE 498/598 PJ

Spring 2022

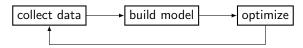
Design of Experiments is focused on process characterization.

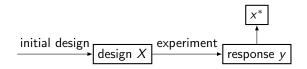
- Which factors affect the response?
- ► How large are the effects?

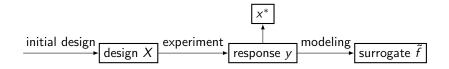
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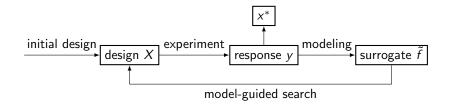
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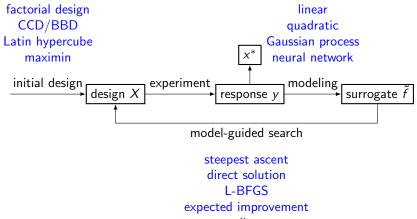
Process improvement asks "what factor settings yield the optimal response?"











rollout

Process improvement by steepest ascent

Rarely are the initial factor ranges optimal. In practice we can be far away.

Process improvement by steepest ascent

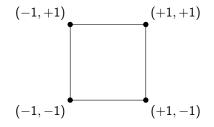
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Process improvement by steepest ascent

- Rarely are the initial factor ranges optimal. In practice we can be far away.
- The method of steepest ascent moves us quickly toward regions of better response.
- The emphasis is on moving quickly using few runs and first order models.

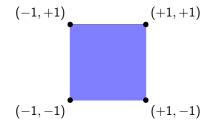
The Design Space

Runs in a factorial design sample the corners of a unit cube.



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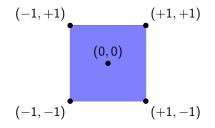
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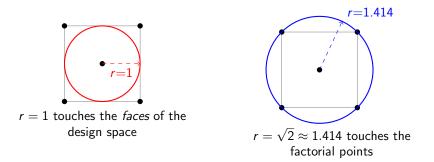
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r = 1 touches the *faces* of the design space

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First-order response surfaces

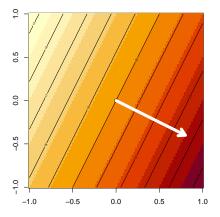
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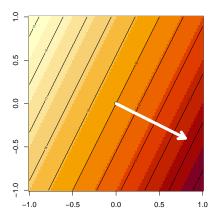
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We want to move "uphill" to improve the response using the **method of steepest ascent**.

If our goal was to minimize the response, we use *steepest descent* by

- 1. Moving opposite of the uphill direction, or
- 2. Multiplying the response by -1.

Finding the ascent direction for first-order models

Let's compute the partial derivatives along each factor's dimension.

$$\frac{\partial y}{\partial x_1} = \frac{\partial}{\partial x_1} \left(20 + 3.6x_1 - 1.8x_2 \right) = 3.6$$
$$\frac{\partial y}{\partial x_2} = \frac{\partial}{\partial x_2} \left(20 + 3.6x_1 - 1.8x_2 \right) = -1.8$$

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Two things to note:

- 1. The rate of ascent along each direction is simply the effect size β_i .
- 2. The rate of change is different for the two dimensions. For every step of unit length along x_1 we must move -1.8/3.6 = -1/2 units along x_2 .

Consider the general first-order model

$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \dots + \beta_n x_n$$

- 1. Find the effect size with the largest **magnitude**. We'll call this β_j and the associated factor x_j .
- 2. Choose a step size (in coded units) along this dimension, called Δx_j .
- 3. For all other dimensions $i \neq j$, the step size is

$$\Delta x_i = \frac{\beta_i}{\beta_j} \Delta x_j$$

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2. Let
$$\Delta x_1 = 1$$
.
3. $\Delta x_2 = \frac{\beta_2}{\beta_1} \Delta x_1 = \frac{-1.8}{3.6} (1) = -0.5$

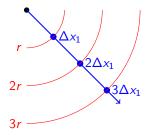
Why standardize step sizes?

Uniform steps give uniform differences in design radii.

 Δx_1 $2\Delta x_1$ $3\Delta x_1$

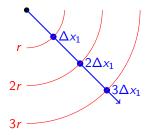
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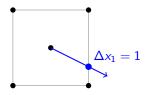


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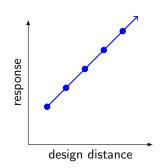
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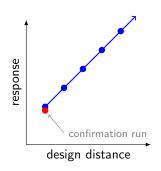
A standardized step of 1 always defines a point on the design space boundary.



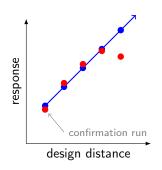
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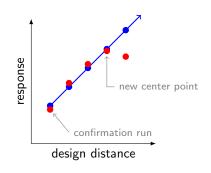
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- Eventually the actual response will stop increasing.
- When the response drifts, we use the best response location as the center for a new set of experiments.



What about interactions?

Models with interactions have **curved** paths of steepest ascent since the gradient changes with x.

$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_{12} x_1 x_2$$
$$\nabla y = \begin{pmatrix} \frac{\partial y}{\partial x_1} \\ \frac{\partial y}{\partial x_2} \end{pmatrix} = \begin{pmatrix} \beta_1 + \beta_{12} x_2 \\ \beta_2 + \beta_{12} x_1 \end{pmatrix}$$

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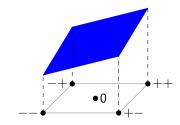
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However, in practice we usually ignore the interactions.

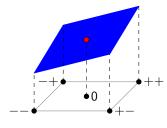
- The model will often break down before the curvature becomes significant.
- We rarely have enough runs in the initial design to identify interactions.

- The FF designs used for process improvement are usually augmented by center points — repeated runs at the design center (0,0).
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 - 1. Estimate the *pure error* via the standard deviation of the repeated runs.
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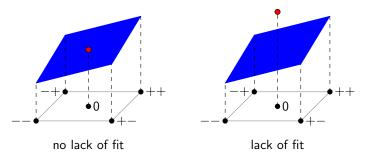


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$$SS_{
m curve} = rac{n_{
m fact} \, n_{
m center} (ar{y}_{
m fact} - ar{y}_{
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m fact} + n_{
m center}}, \quad {
m DF}(SS_{
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3.

2.

$$SS_{error} = \sum_{\substack{\text{center} \\ \text{points}}} (y_i - \bar{y}_{\text{center}})^2, \quad \mathsf{DF}(SS_{error}) = n_{\text{center}} - 1$$

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4.

$$F_{ ext{curve}} = rac{SS_{ ext{curve}}/ ext{DF}(SS_{ ext{curve}})}{SS_{ ext{error}}/ ext{DF}(SS_{ ext{error}})}$$

| temp | time | yield |
|------|------|-------|
| _ | _ | 39.3 |
| _ | + | 40.0 |
| + | _ | 40.9 |
| + | + | 41.5 |
| 0 | 0 | 40.3 |
| 0 | 0 | 40.5 |
| 0 | 0 | 40.7 |
| 0 | 0 | 40.2 |
| 0 | 0 | 40.6 |

1. $\bar{y}_{fact} = (39.3 + 40.0 + 40.9 + 41.5)/4 = 40.425$ $\bar{y}_{center} = (40.3 + 40.5 + 40.7 + 40.2 + 40.6)/5 = 40.46$

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 $\textit{SS}_{curve} = \frac{4 \times 5 \times (40.425 - 40.46)^2}{4 + 5} = 0.0026$

2.

time yield temp 39.3 40.0 +40.9 +— 41.5 ++0 0 40.3 40.5 0 0 0 0 40.7 0 0 40.2 40.6 0 0

| 1. | $\bar{y}_{fact} = (39.3 + 40.0 + 40.9 + 41.5)/4 = 40.425$ | | |
|----|---|------|------|
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| | | _ | _ |
| | $SS_{	ext{curve}} = rac{4 	imes 5 	imes (40.425 - 40.46)^2}{4 + 5} = 0.0026$ | _ | + |
| | 4+5 | + | _ |
| 3. | | + | + |
| | | 0 | 0 |
| | $SS_{ m error} = (40.3 - 40.46)^2 + \dots + (40.6 - 40.46)^2$ | 0 | 0 |
| | = 0.172 | 0 | 0 |
| | | 0 | 0 |
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| | | | |

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| 2. | temp | time | 2 |
| | — | - | |
| $SS_{	ext{curve}} = rac{4 	imes 5 	imes (40.425 - 40.46)^2}{4 + 5} = 0.0026$ | _ | + | |
| 4+5 | + | - | |
| 3. | + | + | 4 |
| ••• (| 0 | 0 | |
| $SS_{ m error} = (40.3 - 40.46)^2 + \dots + (40.6 - 40.46)^2$ | 0 | 0 | |
| = 0.172 | 0 | 0 | |
| | 0 | 0 | |
| 4. 0.0026 /1 | 0 | 0 | 4 |
| $F_{	ext{curve}} = rac{0.0026/1}{0.172/(5-1)} = 0.0605$ | | | |

yield 39.3 40.0 40.9 41.5 40.3 40.5 40.7 40.2 40.6

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|---|------|------|-------|
| $y_{\text{center}} = (40.3 + 40.3 + 40.1 + 40.2 + 40.0)/3 = 40.40$ | temp | time | yield |
| | _ | _ | 39.3 |
| $SS_{ m curve} = rac{4	imes 5	imes (40.425-40.46)^2}{4+5} = 0.0026$ | _ | + | 40.0 |
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| $F_{	ext{curve}} = rac{0.0026/1}{0.172/(5-1)} = 0.0605$ | | | |

pf(0.0605, 1, 4, lower.tail=FALSE) $\rightarrow p < 0.818$.

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- 4. Go to (1) and repeat using the location of maximum response as the new center point.